

# 纯氢内燃机氮氧化物排放机内净化的仿真研究

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**摘要:** 纯氢内燃机工作时不会产生一氧化碳、碳氢化合物等有害排放物, 但会面临高氮氧化物排放的问题, 而机内净化 and 机外净化是控制氮氧化物排放的两种常用手段。机外净化主要通过成熟的选择性催化还原(SCR)技术降低氮氧化物排放, 但机内净化技术目前还很少被关注。为此, 采用 Chemkin Pro 软件中的闭口均质反应器模型来模拟纯氢内燃机氮氧化物排放的机内净化。结果显示, 废气再循环(EGR)技术可以降低氮氧化物排放, 当 EGR 率为 20% 时, 氮氧化物排放降低了 45.3%, 但仅使用 EGR 来降低氮氧化物排放的效果还不够明显, 氮氧化物排放依然很高。与单独应用 EGR 技术相比, EGR 技术与稀薄燃烧技术相结合能够更好地实现氮氧化物排放控制, 如过量空气系数为 1.4、EGR 率为 20% 时, 氮氧化物排放量降低了 96.31%, 实现了纯氢发动机的超低排放。与 EGR 技术以及 EGR-稀薄燃烧技术相比, 内部选择性非催化还原技术的氮氧化物排放控制效果更佳, 仅 10% 的氨气比例就能使纯氢发动机氮氧化物排放降低 96.32%, 15% 的氨气比例可以实现纯氢发动机氮氧化物零排放, 且并不需要 EGR 或稀薄燃烧技术的参与; 然而, 精确控制发动机缸内氨气比例是十分必要的, 否则会产生残氨排放污染环境。

**关键词:** 纯氢内燃机; 氮氧化物排放; 稀薄燃烧; 选择性非催化还原; 废气再循环

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which has been well studied. However, there are few studies on  $\text{NO}_x$  emission control of pure hydrogen engines through inner-engine control. In this paper, the closed homogeneous reactor (CHR) in Chemkin Pro was used to simulate the main inner-engine  $\text{NO}_x$  emission control in pure hydrogen engines. The results show that single exhaust gas recirculation (EGR) decreases  $\text{NO}_x$  emission by 45.3% at an EGR ratio of 20%, indicating that the  $\text{NO}_x$  emission is not significantly reduced. However, EGR plus lean-burn decreases  $\text{NO}_x$  emission by 96.31% at a  $\lambda$  of 1.4 and an EGR ratio of 20%, achieving ultra-low  $\text{NO}_x$  emission of pure hydrogen engines. Compared with single EGR and EGR plus lean-burn, SNCR are better for  $\text{NO}_x$  emission control. A  $\text{NH}_3$  ratio of only 10% can decrease  $\text{NO}_x$  emission by 96.32% on pure hydrogen engines, while a  $\text{NH}_3$  ratio of 15% can achieve zero  $\text{NO}_x$  emission on pure hydrogen engines without a large  $\lambda$  value and EGR ratio. However, it is necessary to accurately control the  $\text{NH}_3$  ratio in the cylinder, otherwise it is easy to produce residual  $\text{NH}_3$  which can pollute the environment.

**Key words:** pure hydrogen engine;  $\text{NO}_x$  emissions; lean-burn; selective non-catalytic reduction (SNCR); exhaust gas recirculation (EGR)

## Simulation of Inner-Engine $\text{NO}_x$ Emission Control on Pure Hydrogen Engines

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**Abstract:** Hydrogen is an ideal engine fuel. Pure hydrogen engines do not produce CO and HC emissions but face the high  $\text{NO}_x$  emission problem. Inner-engine control and outer-engine control are two ways to decrease the  $\text{NO}_x$  emission. Outer-engine control mainly reduce  $\text{NO}_x$  emission through selective catalytic reduction (SCR),

The massive consumption of fossil energy has brought severe pollution problem<sup>[1-2]</sup>. Seeking clean and efficient renewable energy could solve the pollution problem and alleviate energy crisis<sup>[3-4]</sup>. Hydrogen is a kind of renewable fuel whose only combustion product is water, which will not cause any damage to the environment<sup>[5-6]</sup>. Pure hydrogen on engines can almost completely remove CO,  $\text{CO}_2$ , unburned HC emissions, and output higher power than pure gasoline. But  $\text{NO}_x$  emission is the main disadvantage of pure hydrogen engine<sup>[7]</sup>. In order to

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solve the problem of  $\text{NO}_x$  emission, the exhaust gas recirculation (EGR) technology, the EGR plus lean-burn technology, the selective non-catalytic reduction (SNCR) technology, and the selective catalytic reduction (SCR) technology, are currently the main technical means to reduce  $\text{NO}_x$  emission<sup>[8-10]</sup>. Outer-engine control mainly reduces  $\text{NO}_x$  emission through SCR, which has been well studied. The EGR technology, the EGR plus lean-burn technology, and the SNCR technology are the main means of inner-engine  $\text{NO}_x$  emission control at present. However, there are few studies on  $\text{NO}_x$  emission control of pure hydrogen engines through inner-engine control. Therefore, this paper simulated and compared three main inner-engine  $\text{NO}_x$  emission control means of pure hydrogen engines, providing theoretical basis for the choice of technical means on inner-engine to reduce  $\text{NO}_x$  emission of pure hydrogen engines.

## 1 Simulation setup and procedure

The simulation software used in this simulation was Chemkin Pro, and the model was closed homogeneous reactor (CHR). The  $\text{H}_2$  combustion mechanism used in this simulation was the detailed mechanism of hydrogen combustion, the  $\text{NO}_x$  generation mechanism used the improved version of Zeldovitch-mechanism, and the  $\text{NO}_x$  desorption mechanism is provided by Golovitchev<sup>[11-13]</sup>. All the chemical reaction mechanisms in the simulation were verified by extensive experiments, and the experimental results could match the simulation accurately. This simulation simulated three inner-engine  $\text{NO}_x$  emission control technical means, EGR, lean-burn plus EGR and SNCR. In this experiment, five  $\lambda$  values (1, 1.1, 1.2, 1.3, 1.4), five EGR ratios (0, 5%, 10%, 15%, 20%) and five  $\text{NH}_3$  ratios (0, 5%, 10%, 15%, 20%) were set. The EGR ratio is defined in Equation (1), and the  $\text{NH}_3$  ratio is defined in Equation (2). Tab. 1 shows the initial conditions for the closed homogeneous reactor.  $V_x$  represented the volume of  $x$  in the following equations.

**Tab.1 Initial conditions for closed homogeneous reactor**

| Parameters               | Values   |
|--------------------------|--|
| Simulation time/s        | 0.04   |
| Initial temperature/K    | 1000   |
| Initial pressure/MPa     | 0.1  |
| Fuel mixture (. vol)     | $\varphi(\text{H}_2)=100\%$                          |
| Oxidizer mixture (. vol) | $\varphi(\text{O}_2)=21\%; \varphi(\text{N}_2)=79\%$ |
| Added species            | $\text{H}_2\text{O}; \text{N}_2; \text{NH}_3$        |
| Excess air ratio         | 1, 1.1, 1.2, 1.3, 1.4                                |

$$\text{EGR ratio} = \frac{V_{\text{EGR}}}{V_{\text{EGR}} + V_{\text{AIR}} + V_{\text{H}_2}} \quad (1)$$

$$\text{NH}_3 \text{ ratio} = \frac{V_{\text{NH}_3}}{V_{\text{NH}_3} + V_{\text{AIR}} + V_{\text{H}_2}} \quad (2)$$

## 2 Results and discussion

### 2.1 Effect of EGR on $\text{NO}_x$ emission

Fig. 1 shows the effect of EGR on total  $\text{NO}_x$  production rate and  $\text{NO}_x$  emission. As can be seen from Fig. 1, with the increase of the EGR ratio, the peak value of the total  $\text{NO}_x$  production rate and the total  $\text{NO}_x$  emission decrease. When the EGR ratio increases from 0% to 20%, the peak value of the total  $\text{NO}_x$  production rate decreases by 38.52%, 63.93%, 80.33%, and 89.34%, respectively. The total  $\text{NO}_x$  emissions decrease by 11.42%, 22.82%, 34.18%, and 45.30%. The  $\text{NO}_x$  formation conditions are high temperature, oxygen enrichment, and high temperature duration. On the one hand, the increase of the EGR ratio reduces the temperature in the cylinder, and at the same time, the increase of the EGR rate also dilutes the concentration of  $\text{N}_2$  and  $\text{O}_2$ , and reduces the  $\text{NO}_x$  generation rate. Therefore, the use of the EGR technology can effectively reduce  $\text{NO}_x$  emission generated during hydrogen combustion.

### 2.2 Effect of EGR plus lean-burn on $\text{NO}_x$ emission

The EGR ratio was kept at 20% and the excess air ratio was increased from 1 to 1.4 to observe the effect of EGR plus lean-burn on  $\text{NO}_x$  emission. Fig. 2 shows the effect of EGR plus lean-burn on total  $\text{NO}_x$  production rate and  $\text{NO}_x$  emission. It can be observed that the peak value of the total  $\text{NO}_x$  production rate decreased continuously with the increase of  $\lambda$ , but the  $\text{NO}_x$  emission increases first and then decreases when

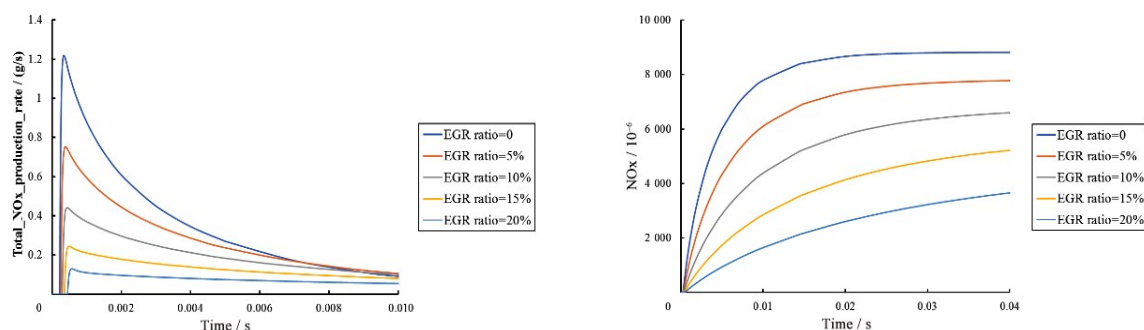


Fig.1 Effect of EGR on total  $\text{NO}_x$  production rate and  $\text{NO}_x$  emission

$\lambda$  increases. At a  $\lambda$  of 1.1, the  $\text{NO}_x$  emission is the highest. Although lean-burn could lower the combustion temperature, a larger  $\lambda$  leads to an increase of  $\text{O}_2$  and creates favorable conditions for the oxygen enrichment, which is conducive to the

generation of  $\text{NO}_x$ . The increase in oxygen results in the fact that the combination of an EGR ratio of 20% with a  $\lambda$  of less than 1.3 cannot effectively reduce the  $\text{NO}_x$  emission. The  $\text{NO}_x$  emission can be reduced by 96.31% when  $\lambda$  is 1.4 and the EGR ratio is 20%.

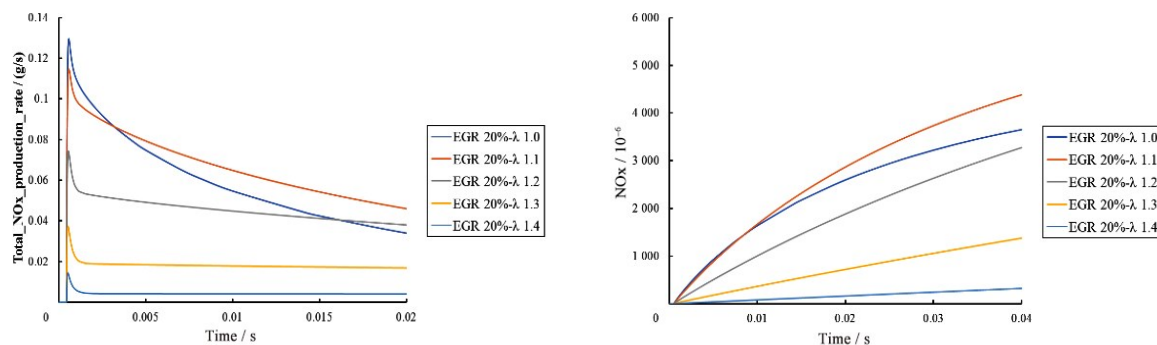


Fig.2 Effect of EGR plus lean-burn on total  $\text{NO}_x$  production rate and  $\text{NO}_x$  emission

### 2.3 Effect of $\text{NH}_3$ on $\text{NO}_x$ emission

Fig. 3 shows the effect of  $\text{NH}_3$  on total  $\text{NO}_x$  production rate and  $\text{NO}_x$  emission. It can be observed that both the positive or negative peak value of the total  $\text{NO}_x$  production rate decrease continuously with the  $\text{NH}_3$  ratio increasing, but the  $\text{NO}_x$  emission decreases with the  $\text{NH}_3$  ratio increasing.

In addition, a larger  $\text{NH}_3$  ratio would lead to a

later peak value of the total  $\text{NO}_x$  production rate. When the  $\text{NH}_3$  ratio is 10%, the  $\text{NO}_x$  emission decreases by 96.32% than without  $\text{NH}_3$  addition while when the  $\text{NH}_3$  ratio is large than 15%, pure hydrogen engines could achieve no  $\text{NO}_x$  emission. However, a large  $\text{NH}_3$  ratio is not recommended, because a large amount of residual  $\text{NH}_3$  will overflow, causing serious pollution to the environment.

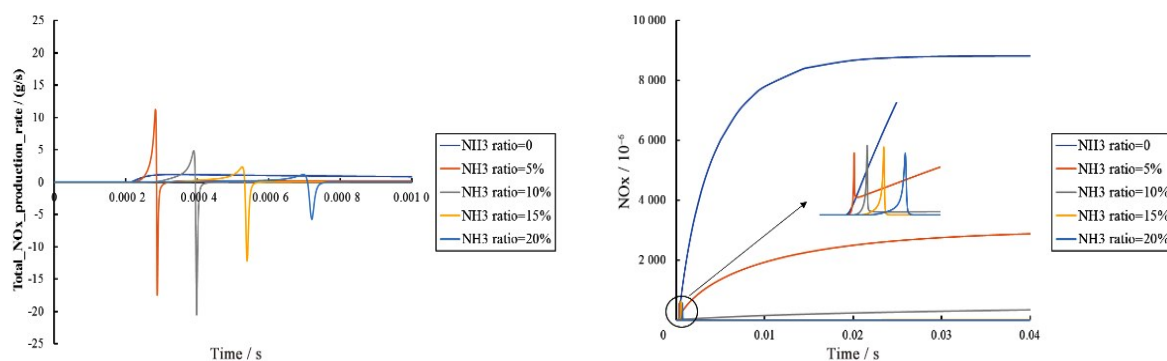


Fig.3 Effect of  $\text{NH}_3$  on total  $\text{NO}_x$  production rate and  $\text{NO}_x$  emission

### 3 Conclusions

This paper used the CHR module in CHEMKIN Pro to simulate the three main means of inner-engine  $\text{NO}_x$  emission control on pure hydrogen engines, providing theoretical guidance for pure hydrogen engines to choose  $\text{NO}_x$  purification means. The main results are as follows:

(1) EGR reduces the  $\text{NO}_x$  emission generated during hydrogen combustion. The  $\text{NO}_x$  emission is reduced only by 45.3% when the EGR ratio is 20%. Therefore, to achieve ultra-low  $\text{NO}_x$  emission using pure hydrogen engines by adopting the EGR technology, a larger EGR ratio or EGR in combination with external purification should be used.

(2) Compared with single EGR, EGR plus lean-burn is more efficient in reducing the  $\text{NO}_x$  emission by using pure hydrogen engines. Pure hydrogen engines need a large EGR ratio and  $\lambda$  value. The  $\text{NO}_x$  emission can be reduced by 96.31% when  $\lambda$  is 1.4 and the EGR ratio is 20%, achieving ultra-low  $\text{NO}_x$  emission of pure hydrogen engines. To control  $\text{NO}_x$  emissions by using pure hydrogen engine and EGR plus lean-burn, the engine condition monitoring should be strengthened to avoid misfire because of the large EGR ratio and  $\lambda$  value.

(3) Compared with EGR, and EGR plus lean-burn, SNCR is better in inner-engine  $\text{NO}_x$  emission control, because it requires only a  $\text{NH}_3$  ratio of 10% to achieve ultra-low  $\text{NO}_x$  emissions on pure hydrogen engines. A  $\text{NH}_3$  ratio a 15% can make pure hydrogen engines achieve zero  $\text{NO}_x$  emission. SNCR avoids pure hydrogen engines having to operate under a large  $\lambda$  and EGR ratio to decrease  $\text{NO}_x$  emission, avoiding the power loss of pure hydrogen engines, making combustion more stable. In the control of  $\text{NO}_x$  emission of pure hydrogen engines, SNCR should be the main technical means to be adopted, and zero emission can be achieved when the proportion of  $\text{NH}_3$  is controlled reasonably.

### References:

- [1] LI D, WANG H, YU X, *et al.* Combustion and emission characteristics of an Acetone-Butanol-Ethanol (ABE) spark ignition engine with hydrogen direct injection[J]. International Journal of Hydrogen Energy, 2021, 46(58): 30145.
- [2] GONG C, YI L, ZHANG Z, *et al.* Assessment of ultra-lean burn characteristics for a stratified-charge direct-injection spark-ignition methanol engine under different high compression ratios [J]. Applied Energy, 2020, 261: 114478.
- [3] ZHEN X, WANG Y. An overview of methanol as an internal combustion engine fuel[J]. Renewable and Sustainable Energy Reviews, 2015, 52: 477.
- [4] THANGAVELU S K, AHMED A S, ANI F N. Review on bioethanol as alternative fuel for spark ignition engines [J]. Renewable and Sustainable Energy Reviews, 2016, 56: 820.
- [5] AYAD S M M E, BELCHIOR C R P, DA SILVA G L R, *et al.* Analysis of performance parameters of an ethanol fueled spark ignition engine operating with hydrogen enrichment [J]. International Journal of Hydrogen Energy, 2020, 45(8): 5588.
- [6] YU X, LI G, DONG W, *et al.* Numerical study on effects of hydrogen direct injection on hydrogen mixture distribution, combustion and emissions of a gasoline/hydrogen SI engine under lean burn condition[J]. International Journal of Hydrogen Energy, 2020, 45(3): 2341.
- [7] KARTHIKEYAN S, PERIYASAMY M. Impact on the power and performance of an internal combustion engine using hydrogen [J]. Materials Today: Proceedings, 2021. <https://doi.org/10.1016/j.matpr.2021.02.356>.
- [8] YU X, ZHAO Z, HUANG Y, *et al.* Experimental study on the effects of EGR on combustion and emission of an SI engine with gasoline port injection plus ethanol direct injection [J]. Fuel, 2021, 305: 121421.
- [9] YU X, GUO Z, HE L, *et al.* Experimental study on lean-burn characteristics of an SI engine with hydrogen/gasoline combined injection and EGR [J]. International Journal of Hydrogen Energy, 2019, 44(26): 13988.
- [10] HE F, YU X, DU Y, *et al.* Inner selective non-catalytic reduction strategy for nitrogen oxides abatement: investigation of ammonia aqueous solution direct injection with an SI engine model[J]. Energies, 2019, 12(14): 2742.
- [11] Ó CONAIRE M, CURRAN H J, SIMMIE J M, *et al.* A comprehensive modeling study of hydrogen oxidation [J]. International Journal of Chemical Kinetics, 2004, 36(11): 603.
- [12] AN H, YANG W M, LI J, *Et al.* Modeling analysis of urea direct injection on the  $\text{NO}_x$  emission reduction of biodiesel fueled diesel engines[J]. Energy Conversion and Management, 2015, 101: 442.
- [13] GOLOVITCHEV V I, MONTORSI L, DENBRATT I. Numerical evaluation of a new strategy of emissions reduction by urea direct injection for heavy duty diesel engines [J]. Engineering Applications of Computational Fluid Mechanics, 2007, 1(3): 189.